

KOSTARCHUK, Viktor Nikolayevich[Kostarchuk, V.M.]; KHATSET, Boris
Isaakovich; KOPERSAK, G.D.[Kopersak, H.D.], red.; VOLKOVA,
N.K., tekhn. red.

[What is possible and what is not possible in geometry using
compass and ruler]Pro mozhlyve i nemozhlyve v geometrii
tsyrkulia i liniiky. Kyiv, Radians'ka shkola, 1962. 124 p.
(MIRA 16:1)

(Geometry)

Link.
KHATSET, F. I.: ~~Master~~ Chem Sci (diss) -- "The effect of the structure of silica
gels on the distribution of mixtures of vapors". Leningrad, 1958. 16 pp (Min
Higher Educ USSR, Leningrad Tech Inst im Leningrad Soviet), 100 copies (KL, No 3,
1959, 108)

KNYAZYUK, K.A.; KHATSET, F.I.; GARKAVENKO, I.P.

Utilizing cold compounds for soil stabilization. Avt. dor. 22 no.9:
6-8 S '59. (MIRA 12:12)
(Soil stabilization) (Bituminous materials)

MASTET F. I.

April 1947

USSR/Silica Gels
Surface Tension

"Effect of Surface Tension of the Coagulant Upon the Formation of the Internal Structure of Silica Gels," I. M. Neumark, F. I. Khatzet, Laboratory of Adsorption Processes, Institute of Physical Chemistry instit N. Y. Pisarshevskiy, Academy of Sciences, USSR, 9 pp

"Kolloidnyy Zhurnal" VOL IX, No 4

Discussion of experimental data, with tables and graphs. Concludes that the surface tension has a considerable effect; the lower the tension, the more coarsely porous types of silica gels are formed, etc. Submitted 20 Dec. 1946. Assistance from Academician N. M. Dubinin and Prof. N. I. Relyakov.

PA 17783

KHATSET, F. I.

PA 35/49TH

USSR/Chemistry - Silica, Colloidal, Aug 48

Chemistry - Silica, Colloidal, Structure

"The Sorption Properties and Structure of Silica Gels," I. Ye. Neymark, F. I. Khatset, R. Yu. Shayfayn, Inst Phys Chem imeni L. V. Pisarzhevskiy, Acad Sci Ukrainian SSR, 4 pp

"Dok Ak Nauk SSSR" Vol LXI, No 6

Studies in authors' laboratory show that conditions of dehydration have decisive influence on gel structure, and pore size of silica gels affects their adsorption capacity. Used samples prepared by previously reported method, based on change in surface

35/49TH

USSR/Chemistry - Silica, Colloidal, Aug 48
Sorption (Contd)

tension of the intermicellar liquid of the gel in process of its dehydration. Pore size was estimated from data of adsorption and desorption of methyl alcohol vapors on evacuated gel samples and of maximum adsorption of aliphatic alcohols from carbon tetrachloride solution. Describes series of samples with increasing pore size. Discusses applicability of M. M. Dubinin's formula to adsorption isotherms for the samples studied. Submitted by Acad M. M. Dubinin, 23 Jan 48.

35/49TH

NEYMARK, I.E.; KHATSET, F.I.

Role of the structure of adsorbents in molecular chromatography
of vapors. Dop. AN URSS no.2:24-29 '49. (MLRA 9:9)

1. Institut fizichnoi khimii im. L.V. Pisarshevs'kogo AN URSS.
Predstaviv diyeniy chlen AN URSS O.I. Brods'kiy.
(Vapors) (Chromatographic analysis)

CA

The phase state of a substance in the adsorbed layer. I. E. Neimark and P. I. Khatset (Inst. Acad. Sci. Ukr. S.S.R., Kiev). *Doklady Akad. Nauk S.S.R.* 74, 751-4 (1950).—The controversial question of the state of aggregation of a vapor physically adsorbed on a solid surface was decided by detns. of the compn. of the mist. adsorbed from a binary mist., as compared with the compn. of the liquid and of the vapor phases of that mist. The answer depends on the type of the porosity of the sorbent. Three types of silica gel, (I) finely porous, (II) medium-porosity, and (III) coarsely porous, preliminarily heated to 400°, were exposed to mixed vapors of C_6H_6 + CCl_4 ; the substance adsorbed was desorbed at 400° until const. wt., and its compn. was detd. On type I, the compn. (at high surface coverage) was found to correspond to that of the vapor, on III mainly to the liquid phase, whereas on II it is intermediate between the two. Consequently, on I the adsorbed substance is gaseous, on III liquid, and on II partly gaseous and partly liquid. At low surface coverages, the adsorbed substance is

gaseous in all cases, and, on I, it remains gaseous over the whole range of coverages. On II and on III, the liquid phase appears at a definite coverage, the later the cover the porosity, e.g. at 0.15 cc./g. on II, and at 0.347 cc./g. on III, and its amt. increases with increasing coverage. Absence of selective adsorption of C_6H_6 from the C_6H_6 + CCl_4 mist. is demonstrated by the constancy of the C_6H_6 content in the substance desorbed from different types of silica gel and its identity with the azeotropic compn. Accordingly, the liquid C_6H_6 + CCl_4 mist. is not sep'd. by filtration through a column of silica gel. In contrast thereto, C_6H_6 is selectively adsorbed on silica gels of type I from a mist. C_6H_6 + C_6H_{10} , i.e. a mist. of mols. of distinctly different sizes. The view ascribing all phys. adsorption to capillary condensation is erroneous; it does not apply at all to finely-porous sorbents, and for coarsely porous sorbents it is true only at sufficiently high surface coverages. Capillary condensation develops when unimol. adsorption is followed by the build-up and merging of multimol. layers in a capillary, and will occur the later the greater the diam. of the pore. N. Thom

DUBININ, M.M., akademik, otvetstvennyy redaktor; GAPON, Ye.N.; GAPON, T.B.;
 ZHYPAKHINA, Ye.S.; RACHINSKIY, V.V.; BELEN'KAYA, I.M.; SHUVAEVA, G.M.;
 ROGINSKIY, S.Z.; YANOVSKIY, N.I.; FUKS, N.A.; KISELEV, A.V.; NEYMARK, I.Ye.;
 SLINYAKOVA, I.B.; KHATSET, P.I.; LOSEV, I.P.; TROSTYANSKAYA, Ye.B.;
 TEVLINA, A.S.; DAVANKOV, A.B.; SALDADZE, K.M.; BRUMBERG, Ye.M.; ZHIDKOVA,
 Z.V.; VEDENEVA, N.Ye.; NAPOL'SKIY, S.A.; MIKHAYLOVA, Ye.A.; KAZANSKIY, B.A.;
 RYABCHIKOV, D.I.; SHEMYAKIN, F.M.; KRETOVICH, V.L.; BUNDEL', A.A.; SAVINOV,
 B.G.; VENDT, V.P.; EPSHTEYN, Ya.A.

[Research in the field of chromatography transactions of the All-Union
 Conference on Chromatography, November 21-24, 1950] Issledovaniya v oblasti
 khromatografii; trudy Vsesoyuznogo soveshchaniya po khromatografii, 21-24
 noiabria 1950 g. Moskva, Izd-vo Akademii nauk SSSR, 1952. 225 p.
 (MLBA 6:5)

1. Akademiya nauk SSSR. Otdelenie khimicheskikh nauk.
 (Chromatographic analysis)

KHATSET, F. I.

Chemical Abstracts
Vol. 48 No. 5
Mar. 10, 1954
General and Physical Chemistry

(4)⁶
The role of structure of adsorbents in molecular chromatography. I. E. Seimark, I. B. Zhurav, and F. I. Khatset. *Izvestiya Akad. Nauk S.S.S.R., Khim. i Mekh. Tsellyul. i Papir. Proizv.* 1953, 1-10 (Pub. 1953). -- Adsorption of C_4H_{10} from solns. in heptane by SiO_2 gel specimens with high or low degrees of porosity showed that selective adsorption of C_4H_{10} takes place only with fine porosity specimens. By repeated adsorption-desorption cycles complete sepn. was readily achieved. The intr. surface area of the adsorbent does not establish the sepn. activity of a given specimen of an adsorbent; the pore structure is the important factor. G. M. Kosolupoff

11-11-54

KNYAZYUK, K.A.; KHATSET, F.I.; CHOBOROVSKAYA, I.S.

Use of heterogeneous soil stabilizing compounds. Avt. dor. 22
no.10:13-15 0 '59. (MIRA 13:2)
(Ukraine--Soil stabilization)

KNYAZYUK, K.A., kand.tekhn.nauk; KHATSET, F.I., kand.tekhn.nauk

Using filter-press waste for soil stabilization. Avt.dor. 25 no.3:
15-16 Mr '62. (MIRA 15:3)

(Soil stabilization)

ATSUTA, R.V.; KHATSET, F.I.; CHOBOROVSKAYA, I.S.

Precise methods of testing soil mixes with organic binding
materials. Avt. dor. 27 no.4:20 Ap '64. (MIRA 17:9)

Alexander Mikhailovich Krivisskii is 60 years old. Ibid.19

KNYAZYUK, K.A., kand.tekhn.nauk; KHATSEY, F.I., kand.tekhn.nauk

Overall soil stabilization using filter-press waste
materials and organic binders. Avt.dor.i dor.stroi.
no.1:164-170 '65. (MIRA 18:11)

KHATSET, I.E.; BENNER, D.P.; BURSHTKYN, I.M.; TUROVSKIY, B.I., red.;
NEMCHENKO, I.Ye., tekhn.red.

[Rights and duties of people building their own dwellings]
Prava i obiazannosti individual'nykh zastroishchikov. Kiev,
Gos.izd-vo lit-ry po stroit. i arkhitekt.USSR, 1958. 158 p.
(MIRA 12:8)

1. Konsul'tatsionnoye byuro Prezidiuma Kiyevskoy oblastnoy
kollegii advokotov (for Khatset, Burshteyn). 2. Glavnyy arbitr
Ministerstva stroitel'stva Ukrainskoy SSR (for Benner).
(Building--Contracts and specifications)

1. Radtsig, I. M., Lyagashenko, S. I.

2. Experiments on inert gases in electric discharges

3. Neon

4. Optika i spektroskopiya, v. 14, no. 1, 1961, p. 1-10

5. Electric discharges in gases, Ne

6. Abstract The investigation was undertaken to determine the data on the properties of the electric discharges in neon.

Card 1, 2

L 9846-63

ACCESSION NR: AP3000576

Addressed. Examination of the material is being conducted by the appropriate authorities.

ACTION: 1-1

PRINTED: 28Sept; DATE ACQ: 10/1/63

ENCL: 1

REF CODE: PH

NR REF SOV: 112

OTHER: 1

18/11

Card 2/2

KUBAL'SKIY, A.P., inzhener; KHATSEVICH, L.I.; OGANOV, S.I.

Practice of manufacturing reinforced concrete supports in the
Tiflis Technical Communication Line Center. Vest.svyazi 16
no.2:22-23 F '56.
(MLRA 9:7)

- 1.Tbilisskiy DRTS (for Kubal'skiy).2.Starshiy tekhnik DRTS (for Khatsevich).
- 3.Starshiy inzhener GUMTS Ministerstva svyazi SSSR.
(Tiflis--Electric lines--Poles)

KARPENKO, V.V., kand.tekhn.nauk, dotsent; KHATSINOV, N.I., kand.tekhn.
nauk, dotsent

Mechanization of grain cleaning and drying barns. Nauch. zap.
KHIMSKH no. 11 Fak. mekh. sel'khoz. 1:27-39 '58. (MIRA 14:3)
(Grain-handling machinery)

KARPENKO, V.V., kand.tekhn.nauk; KHATSINOV, M.I., kand.tekhn.nauk;
TVERSKOY, M.I. [Tvers'kol, M.I.], kand.tekhn.nauk; ZUBKOVA, A.S., inzh.

Grip for removing ensilage. Mekh. sel'. hosp. 9 no.9:20-21 S '58.
(Hoisting machinery) (Ensilage) (MIRA 11:10)

DABAGYAN, Areg Vagarshakovich, doktor tekhn.nauk, dotsent; KHATSINOVA, Ella Naumovna, inzh.

Concurrent electromechanical oscillations of the rotors of turbo-generators and hydrogenerators during steady state nonsymmetrical operation. Izv. vys. ucheb. zav.; elektromekh. 5 no.12:1408-1412 '62.
(MIRA 16:6)

1. Khar'kovskiy politekhnicheskii institut (for Dabagyan).
2. Khar'kov'skiy zavod tyazhelogo elektromashinostroyeniya (for Khatsinova).
(Electric power distribution) (Turbogenerators)

BELOVOL, A.M.; KHATSINSKAYA, A.P.

Workers of the Korenovskaya Sugar Factory are well prepared for the busy season. Sakh. prom. 35 no.12:11-12 D '61. (MIRA 15:1)

1. Korenovskiy sakharnyy zavod.
(Korenovskaya--Sugar industry)

6 1752, -63

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"APPROVED FOR RELEASE: 09/17/2001

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Card 2/4

APPROVED FOR RELEASE: 09/17/2001

CIA-RDP86-00513R000721910015-5"

KHATSIREVICH, I.Kh.

Numerical sequences. Limits of numerical sequences. Uch.zap.Chkal,
gos.ped.inst.no.9:285-322 '56. (MLRA 10:3)
(Numbers, Theory of)

124-58-9-10257

Translation from: Referativnyy zhurnal, Mekhanika, 1958, Nr 9, p 122 (USSR)

AUTHOR: Khatsirevich, I. Kh.

TITLE: On a Method for the Solution of the Plane Problem of the Theory of Elasticity for an Infinite Multiply Connected Region (Ob odnom metode resheniya ploskoy zadachi teorii uprugosti dlya beskonечноy mnogosvyaznoy oblasti)

PERIODICAL: Uch. zap. Chkalovskiy gos. ped. in-t, 1957, Nr 11, pp 221-227

ABSTRACT: A method is given for the first fundamental problem of the theory of elasticity for an infinite multiply connected region. Kolosov's functions $\varphi(z)$ and $\psi(z)$ are sought in the form

$$\begin{aligned} \varphi(z) = & \frac{1}{2\pi i} \int \omega(t) \ln(t-z) ds + \\ & + \sum_{j=1}^m a_j \ln(z-z_j) + \sum_{j=1}^m \frac{b_j}{z-z_j} \end{aligned} \quad (1)$$

Card 1/2

124-58-9-10257

On a Method for the Solution of the Plane Problem (cont.)

and

$$\psi(z) = -\frac{1}{2\pi i} \int_L \overline{\omega(t)} \ln(t-z) ds - \frac{1}{2\pi i} \int_L \frac{\omega(t) \bar{t}}{t-z} ds + \sum_{j=1}^m \frac{b_j}{z-z_j} \quad (2)$$

The author obtains an integral equation for the unknown function $\omega(t)$, for which he demonstrates the existence and uniqueness of a solution. The representation of the stress functions by means of formulas (1) and (2) assumes that the stresses go to zero at infinity.

V. I. Mossakovskiy

1. Elasticity--Theory 2. Mathematics--Applications

Card 2/2

KHATSIREVICH, M. (g.Prokop'yevsk Kemerovskoy oblasti)

Simple method for a laboratory synthesis of silver nitrate. Khim.
v shkole 15 no.6;81 M-D '60. (MIRA 13:11)
(Silver nitrate)

KHATSIREVICH, M. G.

Bee Culture

Winter care of bees. Pchelovodstvo 30, No. 2, 1953.

9. Monthly List of Russian Accessions, Library of Congress, June 1953, Uncl.

KHATSIREVICH, M.G., uchitel'

School collection of minerals and products obtained from them,
exhibited in glass-enclosed cases. Khim.v shkole 15 no.1:
85-87 Ja-P '60. (MIRA 13:5)

1. Srednyaya shkola No.18 goroda Prokop'yevska.
(Mineralogy--Collecting of specimens)

ZIKEYEVA, A.I.; KREPKOGORSKAYA, T.A., doktor meditsinskikh nauk; KHATSKELES,
A.Ya.

Pathomorphology of experimental leptospiral fever induced by *Leptospira*
of the Kazakhstan type. Vest.AN Kazakh.SSR 17 no.4:29-37 Ap '61.
(Kazakhstan—Leptospirosis) (MIRA 14:5)

ZIKEYEVA, A.I., dotsent; KHATSKELES, A.Ya.

Causes of death among middle aged and aged subjects. Zdrav.
Kazakh. 22 no.3:33-39 '62. (MIRA 15:12)

1. Iz kafedry patologicheskoy anatomii (zav. - prof. P.P.Ochkur)
Kazakhskogo meditsinskogo instituta.
(DEATH--CAUSES) (AGFD)

KHATSKELEVICH, M.N.; MELENT'YEV, A.A.; SIBAROV, V.D.; SERGEYEV, Ye.S.,
redaktor; KHITROV, P.A., tekhnicheskiiy redaktor.

[Problems of improving the technical aspects of shunting station
operations] Voprosy uluchsheniia tekhnologicheskikh protsessov ra-
boty sortirovochnykh stantsii. Moskva, Gos. transp. zheleznodorozh.
izd-vo, 1952. 230 p. [Microfilm] (MLRA 7:11)
(Railroads--Making up trains)

AKSENOV, I.Ya.; SUYAZOV, I.G.; GORODNICHIEV, N.G., redaktor; KHATSKE-
LEVICH, M.N., redaktor.

[Manual for learning rules of the technical operation of rail-
roads in the Soviet Union] Posobie dlia izucheniia pravil tekhnicheskoi
ekspluatatsii shelesnykh dorog Soiuzs SSR. 7 izd., perer.
i dop. Moskva, Gos. transp. i shel-dor izd-vo, 1954. 614 p.
(Railroads) (MIRA 7:8)

AKSENOV, Ivan Yakovlevich; SUYAZOV, Ivan Grigor'yevich; KHATSKHELEVICH, M.N.,
redaktor; TSARENKO, A.P., redaktor; VERINA, G.P., ~~tekhnicheskii~~
redaktor

[A manual for the study of the principles of the technical operation
of Soviet railroads] Posobie dlia izucheniia pravil tekhnicheskoi
ekspluatatsii zheleznykh dorog Soiuza SSR. Izd. 2-oe, perer. i dop.
Moskva, Gos. transp.zhel-dor. izd-vo, 1956. 482 p. (MIRA 10:1)
(Railroads--Management)

KHATSKELEVICH, M.N., inzh.

New engineering specifications for railroads in the U.S.S.R.
Zhel. dor. transp. 41 no.4:9-15 Ap '59. (MIRA 12:6)
(Railroads--Specifications)

KHATSKHELEVICH, M.N., otv. za vypusk; VERINA, G.P., tekhn.red.

[Rules for the technical operation of railroads in the U.S.S.R.]
Pravila tekhnicheskoi ekspluatatsii zheleznykh dorog Soiuza SSR.
Moskva, Gos.transp.zhel-dor.isd-vo, 1960. 145 p. (MIRA 13:4)

1. Russia (1923- U.S.S.R.) Ministerstvo putey soobshcheniya.
(Railroads--Management)

KHATSKELEVICH, M.N., otv. za vypusk; VERINA, G.P., tekhn.red.

[Regulations on railroad signaling in the U.S.S.R.] Instruktsiia po signalizatsii na zheleznykh dorogakh Soiuza SSR. Moskva, Gos.transp.zhel.-dor.izd-vo, 1960. 172 p.

(MIRA 13:7)

1. Russia (1923- U.S.S.R.) Ministerstvo putey soobshcheniya.
(Railroads--Signaling)

OSIPOV, S.I., inzh.; KHATSKELEVICH, M.N., inzh.

Replies to readers' questions. Elek. i tepl. tiaga 4 no.1:45

Ja '60.

(MIRA 13:4)

(Railroads--Maintenance and repair)

DANTIOV, V.I., inzh.; KHATSKHEVICH, M.M., inzh.; CHERNYSHEVICH, F.I.,
inzh.

Reply to the inquiries of our readers. Elek. i tepl. tiaga 4 no.5:
44 My '60. (MIRA 13:7)
(Electric railway motors) (Railroads--Signaling)

KONOVALOV, N.A.; DANILOV, V.I., inzh.; KHATSKHELEVICH, M.N., inzh.

Reply to the inquiries of our readers. Elek.i tepl.tiaga. 4
no.6:42-43 Jo '60. (MIRA 13:8)

1. Master motorno-apparatnogo tsekha depo Moskva III Moskovskoy
dorogi.

(Electric locomotives--Maintenance and repair)
(Diesel locomotives)
(Railroads--Signaling)

GORN, V.N., inzh.; KLIMOV, M.N., inzh.; DANILOV, V.I., inzh.;
KHATSKELEVICH, M.N., inzh.

Reply to the inquiries of our readers. Elek. i tepl. tiaga 4
no. 9:44 S '60. (MIRA 13:12)
(Railroads--Signaling) (Diesel locomotives)

. KHATSKHELEVICH, M.N., inzh.; DANILOV, V.I., inzh.

Reply to the inquiries of our readers. Elek. i tepl. tiaga 4 no.11:
42 N '60. (MIRA 13:12)

(Railroads--Signaling)

BAKSHANSKAYA, R.S.; KHATSKELEVICH, M.N., nauchnyy tekhn. red.; RODOVSKAYA, M.V., otv. za vypusk; VOROTNIKOVA, L.F., tekhn. red.

[Mechanization and automation in the classification yards of U.S.S.R. and foreign railroads; bibliographic index of Soviet literature published from 1955 to 1960] Mekhanizatsiia i avtomatizatsiia na sortirovochnykh stantsiiakh zheleznykh dorog v SSSR i za rubezhom; bibliograficheskii ukazatel' otechestvennoi literatury 1955-1960 gg. Moskva, Vses. izdatel'sko-poligr. ob"edinenie M-va putei soobshcheniia, 1961. 14 p. (MIRA 14:10)

1. Russia (1923- U.S.S.R.) Ministerstvo putey soobshcheniya. Tsentral'naya nauchno-tekhnicheskaya biblioteka.
(Bibliography--Railroads--Yards) (Automatic control)

KHATSEBLEVICH, M.N., inzh.; FAYNGOL'D, I.Ya., inzh.; BOROVSKII, G.M.,
kand.tekhn.nauk; KLIMOV, M.N., inzh.

Replies to the inquiries of our readers. Elek. i topl. tsiaga
5 no.5:43 My '61. (MIRA 14:7)

(Railroads--Signaling)

(Diesel locomotives--Maintenance and repair)

YURCHENKO, I.F.; GORN, V.N., inzh.; KLIMOV, N.N., inzh.; KHATSKELEVICH,
M.N., inzh.

Replies to the inquiries of our readers. Elek. i tepl. tiaga
5 no.8:42-44 Ag '61. (MIRA 14:9)

1. Nachal'nik Upravleniya truda, zarplaty i tekhniki bezopasnosti
Ministerstva putey soobshcheniya (for Yurchenko).
(Railroads--Brakes) (Locomotives)

KHATSKELEVICH, M.N., inzh.; ZAV'YALOV, G.N.; NOVIKOV, A.V., inzh.;
OZOLIN, A.K., inzh.; LAPIN, V.B., inzh.; DANILOV, V.I., inzh.

Replies to the inquiries of our readers. Elek.i tépl.tiaga 5
no.9:45-46 S '61. (MIRA 14:10)

1. Glavnyy tekhnolog po avtotormozam Glavnogo upravleniya
lokomotivnogo khozyaystva Ministerstva putey soobshcheniya (for
Zav'yalov).

(Railroads---Brakes) (Diesel locomotives)
(Insulating oils)

RADCHENKO, V.D., kand.tekhn.nauk; PERTSOVSKIY, L.M., inzh.;
KHATSKELEVICH, M.N., inzh.; KLIMOV, N.N., inzh.; GROMOV, S.A.,
~~kand.tekhn.nauk~~

Answering readers' queries. Elek.i tepl.tiaga 5 no.11:43-44 N '61.
(MIRA 14:11)

(Electric locomotives)

(Diesel locomotives)

PUSHKAREV, I.F., inzh.; STREKOPYTOV, V.V., inzh.; KOVRIZHKIN, N.P., inzh.;
KURBATOV, A.I., proyemshchik; KHATSKELEVICH, M.N., inzh.

Answering readers' queries. Elek.i tepl.tiaga 6 no.4:36-37
Ap '62. (MIRA 15:5)

1. Lokomotivnoye depo Leningrad-Baltiyskiy (for Kurbatov).
(Locomotives)

YURCHENKO, I.F.; KHATSKELEVICH, M.N., inzh.; TOLKACHEV, V.P., inzh.;
KLIMOV, N.N., inzh.; MATVEYEV, P.M.; NOVIKOV, A.V., inzh.

Answers to readers' queries. Elek.i tepl.tiaga 6 no.2:44-45
F '62. (MIRA 15:2)

1. Nachal'nik upravleniya truda, zarabotnoy platy i tekhniki bezopasnosti Ministerstva putey soobshcheniya (for Yurchenko).
2. Direktor Vsesoyuznogo nauchno-issledovatel'skogo instituta zheleznodo-rozhnoy gigiyeny Glavnogo sanitarnogo upravleniya Ministerstva putey soobshcheniya (for Matveyev).
(Railroads)

REBRIK, B.N., kand.tekhn.nauk, starshiy nauchnyy sotrudnik; ZAV'YALOV, G.N.;
VASHURIN, A.A., inzh.; KHATSKELEVICH, M.N., inzh.

Answering readers queries. Elek. i tepl.tiaga 6 no.8:42-44
Ag '62. (MIRA 17:3)

1. Otdeleniye elektrifikatsii Vsesoyuznogo nauchno-issledovatel'skogo
instituta zheleznodorozhnogo transporta Ministerstva putey
soobshcheniya (for Rebrik). 2. Glavnyy tekhnolog po avtotormozam
Glavnogo upravleniya lokomotivnogo khozyaystva Ministerstva putey
soobshcheniya (for Zav'yalov).

PUSHKAREV, I.F., inzh.; ZASLAVSKIY, G.N.; KUZNETSOV, T.F., starshiy
nauchnyy sotrudnik; KHATSKHELEVICH, M.N., inzh.

Replies to the inquiries of our readers. Elek. i tepl.
tiaga 6 no.10:35-36 0 '62. (MIRA 15:11)

1. Zaveduyushchiy bazovoy teplovoznoy laboratoriyey
Khar'kovskogo instituta inzhenerov zheleznodorozhnogo
transporta in. Kirova (for Zaslavskiy).

(Diesel locomotives)
(Railroads--Rolling stock)

DUBROVSKIY, Z.M., inzh.; GUREVICH, A.N., kand.tekhn.nauk; KHATSKELEVICH,
M.N., inzh.

Replies to the inquiries of our readers. Elek. i tepl. tiaga
6 no.11:42-43 N '62. (MIRA 16:1)
(Electric locomotives) (Diesel locomotives)

KHATSKELEVICH, M.N., inzh.; KLIMOV, N.N., inzh.

Replies to the inquiries of our readers. Elek.1 tepl.tiaga 7
no.2:42 F '63. (MIRA 16:2)
(Railroads—Signaling—Centralized traffic control)

DZHAVAKHAYN, T.V., inzh.; KIDALINSKIY, L.P.; KHATSKELEVICH, M.N.,
inzh.; KLIMOV, N.N., inzh.

Reply to the inquiries of our readers. Elek. i topl. tiaga 7
no.3:36-37 Mr 163. (MIRA 16:6)

1. Glavnyy inzh. Muromskogo zavoda im. F.E. Dzerzhinskogo
(for Kidalinskiy).
(Electric railroads)

ZAV'YALOV, G.N.; KRYLOV, V.I.; OZOLIN, A.K.; RUDKOV, G.V.; KHATSKHELEVICH, M.N.,
inzh.

Replies to the inquiries of our readers. Elek.i tepl.tiaga 7
no. 1243-44, Ja '63. (MIRA 1642)

1. Glavnyy tekhnolog po avtotormosam Glavnogo upravleniya lo-
motivnogo khozyaystva Ministerstva putey soobshcheniya (for Zav'-
yalov). 2. Nachal'nik tormoznoy laboratorii Moskovskogo tormoznogo
zavoda (for Krylov). 3. Zamestitel' nachal'nika spetsial'nogo
konstruktorskogo byuro Moskovskogo tormoznogo zavoda (for Ozolin).
4. Zamestitel' nachal'nika proyektno-tekhnologicheskogo otdela po
remontu i ekspluatatsii teplovozov pri zavode im. Il'icha (for
Rudkov).

(Railroads--Signaling)

(Diesel locomotives)

KHATSKELEVICH, M.N., inzh.; KLIMOV, N.N., inzh.; NIKANOROV, V.A.

Replies to the inquiries of our readers. Elek. i tepl. tiaga '7
no.4:40 Ap '63. (MIRA 16:5)

1. Glavnyy inzhener Glavnogo upravleniya lokomotivnogo khozyaystva
Ministerstva putey soobshcheniya (for Nikanorov).
(Railroads--Rolling stock)

KLIMOV, N.N., inzh.; PROKHOROV, A.A.; KHATSKELEVICH, M.N., inzh.; SAVEL'YEV, A.A.,
inzh.

Answering readers' queries. Elek. i tepl.tiaga 7 no.11:44 N '63.

(MIRA 17:2)

1. Glavnyy sanitarnyy vrach zheleznodorozhnogo transporta Ministerstva
putey soobshcheniya (for Prokhorov).

KHATSKHELEVICH, S.Ya. (Moskva, G-34, per. Ostrovskogo, d.20, kv. 7)

Case of osteoplastic sarcomatocarcinoma of the thyroid gland. Nov. khir.
arkh. 5 no.:117-118 6-0 '58. (MIRA 12:1)

1. Khirurgicheskoye otdeleniye 30-y Moskovskoy gorodskoy bol'nitsy
(nauchnyy rukovoditel' - doktor med. nauk S.S. Avedisov).
(THYROID GLAND--SURGERY)

KHATEKELEVICH, S.Ya. (Moskva, pereulok Ostrovskogo, d.10 kv.7)

Nitrous oxide anesthesia under polyclinical conditions. Vest.
khir. 91 no.9:97-100 S'63. (MIRA 17:4)

1. Iz khirurgicheskogo otdeleniya (zav. - doktor med. nauk S.S. Avedisov) 30-y bol'nitsy i 34-y polikliniki (zav. otdeleniyem - I.M. Osnos, nauchnyy rukovoditel' - prof. I.S. Zhorov) Moskvyy.

AYEDISOV, S.S., doktor med.nauk (Moskva, K-9, ul. Stanislavskogo, d. 12, kv.17)
~~..KHATSKHEVICH, S.Ya.~~

Late posttransfusion complications in Rh incompatibility. Vest.khir.
81 no.8:100-101 Ag '58 (MIRA 11:9)

1. Iz khirurgicheskogo otdeleniya gorodskoy bol'nitsy No.30
g. Moskvyy (gl. vrach M.L. Belyayeva).
(RH FACTOR

incompatibility in blood transfusion (Rus))
(BLOOD TRANSFUSION, compl.
posttransfusion reaction caused by Rh incompatibility (Rus)

AVEDISOV, S.S., doktor med.nauk; KHATSKELEVICH, S.Ya.

Benign nonepithelial tumors of the stomach. Sov.med. 25 no.1:108-
115 Ja '61. (MIRA 14:3)

1. Iz khiurgicheskogo otdeleniya (zav. - doktor med.nauk S.S.Avedisov)
30-y gorodskoy bol'nitsy Moskvy (glavnyy vrach N.L.Belyayeva).
(STOMACH—TUMORS)

L 22713-66 EWT(1)/EWA(h)

ACC NR: AP6002933 (A)

SOURCE CODE: UR/0286/65/000/024/0102/0102

AUTHORS: Khatskelevich, Ya. D.; Bulatov, V. K.; Popov, S. A.; Mityakov, A. I. 17

ORG: none

TITLE: A trigger for controlling relay-contact commutators. Class 42, No. 177159

SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 24, 1965, 102

TOPIC TAGS: relay system, electronic circuit reliability, commutator

ABSTRACT: This Author Certificate presents a trigger for controlling relay-contact commutators. The trigger contains transistors with the windings of the relay in their collector circuit. The design increases the reliability of the trigger and reduces its response time. The bases of the transistors are connected with the contacts of one of the relays. This relay connects the input of the trigger to the bases of the transistors (see Fig. 1). The emitters of the transistors are joined together and are connected to the voltage source through a resistance and the contacts of the second relay. Diodes are connected between the base and the emitter of each transistor.

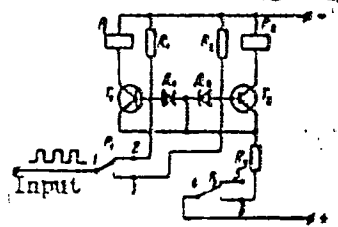
Cord 1/2

UDC: 681.142:621.374.3 2

L 22713-66

ACC NR: AP6002933

Fig. 1. P_1 and P_2 - Relays; T_1 and T_2 - transistors;
 D_1 and D_2 - diodes; R_1 , R_2 and R_3 - resis-
 tors; 1-3 - contacts of relay P_1 ;
 4-6 - contacts of relay P_2 .



Orig. art. has: 1 figure.

SUB CODE: 09/ SUBM DATE: 14May64

Card 2/2

KHATSKELEVICH, V. A.

10" THE APPLICATION OF NEGATIVE FEEDBACK TO RADIO
TRANSMITTERS USING GRID MODULATION. S. V.
Person A. V. Khatskelevich (Izvestiya Elektro-
techn. Nauk, No. 12, 1969, pp. 11-24)

The possibility is discussed of introducing negative feedback into grid modulated transmitters already in operation in Russia. Various types of feedback (over the modulator channel, over the modulated high-frequency signal, and over both the high-frequency and low-frequency channels) are considered. Phase and phase-frequency distortions thus introduced are examined, and measures to reduce these are suggested. The possibility of self-excitation of the transmitter is discussed in detail, and in conclusion a brief report is given on an experimental investigation in which feedback over the high-frequency and low-frequency channels was employed.

KHATSKHELEVICH, V. A.

PA 30/49T103

USSR/Radio
Antennas - Constants
Resonance

Nov/Dec 48

"Investigation of Resonance and Asymmetry in Edkok's
Antenna-Feeder System," A. Z. Fridin, V. A. Khatskel-
evich, Candidates Eng Sci, 22 1/2 pp

"Radiotekhn" Vol III, No 6

Presents sufficiently accurate investigation of reso-
nance phenomena which occur in an Edkok ¹⁷/_{Edcock} 17/
asymmetrical antenna-feeder system. Results enable
some important amendments to existing concepts of
these phenomena. Presents detailed investigation of
the influence of asymmetry of individual elements of

30/49T103

USSR/Radio (Contd.)

Nov/Dec 48

the system on its resonances, and on distortions of
the direction diagram. Analysis of the latter en-
ables nature and magnitude of errors in operation
of Edkok antenna-feeder systems, e.g., in direction
finders, to be determined. Submitted 12 Jul 48.

30/49T103

KHATSKOLEVICH, V. A. (Co-author)

See: PERSON, S. V.

Person, S. V. and Khatskelevich, V. A. - "Dynatron generation in:
high-power high- and low-frequency amplifiers and methods of
combatting it," Sbornik trudov Leningr. elektrotekhn. in-ta
svyazi im. S.Bonch-Bruyevicha, Issue 4, 1949, p. 14-29

SO: U-3566, 15 March 53, (Letopis 'Zhurnal 'nykh Statey, No. 14, 1949).

KHATSKELEVICH, V. A. and FRADIN, A. Z.

"Symmetrical and Asymmetrical Adcock Antenna Feeder Systems," Sbornik Trudov
LEIS imeni Bonch-Bruyevich, No 6, 1949.

TEORIYA I RASCHET STABILNOY
LAMPOVYKH TSIKLOV

Theory and Design of
Voltage-Mode Power Amplifiers

by V.V. Pershin, A.I. Lobachev
V.A. Isachenkov

Published by "Sovetskoye Radio"

The authors of the book are
engineers, who have worked in the
theory and design of power
amplifiers, and model them in
general, and model them in
a number of years of work
contributed to the theory of
amplitude-modulated signals
the present work.

1. The first part of the document is a list of the names of the persons who were present at the meeting. The names are listed in alphabetical order. The names are: [illegible]

2. The second part of the document is a list of the topics that were discussed at the meeting. The topics are listed in alphabetical order. The topics are: [illegible]

3. The third part of the document is a list of the actions that were taken at the meeting. The actions are listed in alphabetical order. The actions are: [illegible]

4. The fourth part of the document is a list of the decisions that were made at the meeting. The decisions are listed in alphabetical order. The decisions are: [illegible]

5. The fifth part of the document is a list of the recommendations that were made at the meeting. The recommendations are listed in alphabetical order. The recommendations are: [illegible]

without grid current
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original section dealing with several types

power amplifiers is given in Table 1.

Table 1. Wavelengths

Wavelength, nm

1000

1000

1000

1000

1000

1000

1000

1000

KHATSKOLEVICH, V.A.; SHUR, L.M.

Envelope negative feedback in radio transmitting apparatus.

Elektrosvyaz' 10 no.11:15-24 N '56.

(MLRA 9:12)

(Radio--Transmitters and transmission)

KHATSKELEVICH, V. A.

CIRCUITS

"Construction of Envelope Feedback Loops in Radio Transmitting Apparatus," by V.A. Khatskelevich, L.M. Shur, Elektrosvyaz', No 7, July 1957, pp 26-33

Problems involved in the design of transmitter circuits with envelope feedback are considered, and the choice of the element of the feedback loop is analyzed. Some ideas are presented concerning a procedure for correcting the frequency characteristics of the loop so as to obtain effective envelope feedback. This work is a continuation of an article published by the authors in the November 1956 issue of Elektrosvyaz'

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APPROVED FOR RELEASE: 09/17/2001

CIA-RDP86-00513R00072191001

AUTHORS: Khatskelevich, V.A. and Shur, L.M.

TITLE: Compensation of Non-linear Distortions by Envelope Feedback in Radio-transmitting Equipment (Kompensatsiya nelineynykh iskazheniy protivosvyaz'yu po ogibayushchey v radioperedayushchikh ustroystvakh)

PERIODICAL: Elektrosvyaz', 1958, Nr 4, pp 8 - 15 (USSR).

ABSTRACT: Non-linear distortions in transmitting equipment are approximately compensated by feedback only at low and medium modulating frequencies. The degree of this approximation depends on the shape of the modulation characteristic which determines the spectrum of the original distortions and the possibility of their compensation by feedback (Refs 1 and 2). Compensation of non-linear distortions is worse at high modulating frequencies and the greater the unevenness of the amplitude-frequency characteristic in the modulation frequency band, the worse the compensation. Under unfavourable conditions, feedback can increase the distortions even with a uniform amplitude-frequency characteristic. The amplitude-frequency characteristic of equipment with feedback (Figure 1) is first considered in its general form.

1) Starting with the formula for the transfer coefficient of

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Compensation of non-linear Distortions by Envelope Feedback in
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apparatus with feedback:

$$\dot{k}_n = \frac{\dot{k}}{1 - \dot{k}\dot{\beta}}$$

and assuming that the degree of feedback is large
($|\dot{k}\dot{\beta}|_p \gg 1$), the characteristic can be given as:

$$y = \left| \frac{\dot{k}_n}{\dot{k}_{np}} \right| \approx \left| \frac{\dot{k}}{\dot{k}_p} \right| \frac{|\dot{k}\dot{\beta}|_p}{|1 - \dot{k}\dot{\beta}|} , \quad (1)$$

where the index p refers to values appertaining to the
mid-frequency of the working band.

The loop frequency characteristic can be formed in circuit \dot{k}
or $\dot{\beta}$, or in both circuits simultaneously and the charac-
teristic will depend on which circuit of the loop is used to
form the "cut-off" (Refs 3, 6).

Thus, if the cut-off is formed by the $\dot{\beta}$ -circuit only, then
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$$|k| = |k|_p = \text{const.}$$

and

$$y = \frac{|k\beta|_p}{v} \quad (3)$$

where

$$v = \left\{ 1 + \left(\frac{|k\beta|_p}{z} \right)^2 + 2 \frac{|k\beta|_p}{z} \cos [180^\circ(1 - a)] \right\}^{1/2}$$

$$z = (x + \sqrt{x^2 - 1})^{2(1-a)}, \quad x = f/f_0,$$

f_0 = the highest modulation frequency of the working band,

$a = \psi/180^\circ$ where ψ is the phase stability margin.

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When the cut-off is formed in the k -section only, i.e.
when the β -circuit is not frequency conscious, we have:

$$|\beta| = |\beta|_p = \text{const}, |k| = \frac{|k|_p}{z}$$

and:

$$y = \frac{1}{z} \frac{|k\beta|_p}{v} \quad (4)$$

The author also shows how the amplitude-frequency characteristic of the circuits k and β can be obtained to give any particular shape of the overall amplitude-frequency characteristics with feedback.

2) Frequency characteristics for the apparatus, calculated by Formulae (3) and (4) with $|k\beta|_p = 10$ and $a = 1/6$

($\psi = 30^\circ$) are produced in Figure 2. From Figure 2, it is seen that a peak occurs at frequencies near to $2f_0$, the

Card4/17 value of which is much greater when the cut-off is formed by the

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β -circuit (Curve 1) than when it is formed by the k -circuit (Curve 2). This fact is significant because in all practical cases, the modulating input voltage contains non-linear distortions. If, for example, the coefficient of the second harmonic of the input voltage at the highest working frequency comprises 1%, then when the cut-off is formed by the β -circuit, the corresponding voltage at the output becomes 20%, but when the cut-off is formed by the k -circuit, the corresponding output voltage is 2% only, the apparatus itself being considered perfectly linear in both cases.

It is obvious that, other conditions being equal, apparatus with the smallest peak in the amplitude-frequency characteristic beyond the limit of the working band, or with a falling characteristic in this region, is preferable. However, to reduce the distortions, it is not necessary to demand that the amplitude-frequency characteristic of the apparatus should not have a large peak or should be falling. This would introduce practical difficulties in its realisation. The problem is more easily solved by connecting in a filter ϕ to limit the frequency band of the input voltage (Figure 1b). Because such

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a filter is not included in the feedback loop, the attenuation which it introduces at frequencies $f > f_0$ can be made sufficiently great to compensate for any rise in the amplitude-frequency characteristic of the apparatus.

3) The author next examines the effect of amplitude characteristics of parts of the loop and of the entire apparatus with feedback beyond the limits of the working band on non-linear distortions arising in the k-circuit (Figure 1b). The k-circuit here consists of two sections; linear k_1 and non-linear k_2 . Non-linear distortions, arising in k_2 ,

can be replaced by a "distortion generator" e_u , connected to the input to this part of the loop. It is assumed that the level of the useful output voltage u_{out} , the e.m.f.

e_u of the distortion generator and the voltage u_{in} at the input to k_2 remain constant and for simplicity only one distortion component is considered. Then:

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$$k_f = \frac{|k_2| e_u}{|k_2|_p u_{Bx}} = y_2^N \text{ and } k_{fn} = \frac{|k_2|}{|1 - k_1 k_2 \beta|} e_u = \frac{|k_2|}{|k_2|_p u_{Bx}} = y_2^N \frac{1}{|1 - k_1 k_2 \beta|} \quad (7)$$

where $N = e_u / u_{Bx}$ is the coefficient giving the degree of non-linearity of the k_2 circuit; k_f and k_{fn} are coefficients of non-linear distortions at the output with and without feedback, respectively; $y_2 = |k_2| / |k_2|_p$ is the

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amplitude-frequency characteristic of the k_2 circuit.

Thus, non-linear distortions at high frequencies depend on the frequency characteristic of the k_2 circuit in which

they arise. Other conditions being equal, they will be less, the more sharply y_2 falls beyond the limits of the working frequency band.

Extra circuits with falling amplitude characteristics, connected after the apparatus, also reduce non-linear distortions at the output. In power modulators, a π -type low-frequency filter, formed by shunting the primary winding of the modulation transformer with a capacitor, would be such a circuit.

Assuming that the loop transfer coefficient $k\beta = k_1 k_2 \beta$ changes according to a step cut-curve and using the previous denotations, from Eq.(7) we get:

$$k_{fn} = \frac{y_2^N}{v} \quad (8)$$

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Eq.(8) shows that k_{fn} does not depend on the amplitude-frequency characteristic of the k_1 and β -circuits.

Therefore, distribution of correcting circuits between these parts of the loop will have no effect on the non-linear distortions.

4) To evaluate the feedback action, it is sufficient to compare non-linear distortions with feedback to distortions in the apparatus without feedback, other conditions remaining equal. The action of feedback on each component of the non-linear distortions can be obtained from Eq.(7) in the form:

$$D_m = \left(\frac{k_{fn}}{k_f} \right)_m = \frac{1}{|1 - k\beta|_m} \quad (9)$$

where the index m denotes the number of the modulation frequency harmonic under consideration.

Eq.(9) remains true for all modulation frequencies. It shows that compensation of non-linear distortions by feedback

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does not depend on the amplitude-frequency characteristics of the parts of the loop k_1 , k_2 , β and of the entire apparatus but is determined by the loop transfer coefficient only, - $k_1 k_2 \beta = k\beta$.

Using the equation for a step dislocation, from Eq.(9) can be found the relationship of the degree of compensation of distortion D_m on the modulating frequency. Two cases are distinguished:

a) the frequency of the harmonic concerned ω equals or is less than ω_0 . In this case, $|k\beta| = |k\beta|_p$ and with deep feedback, we obtain:

$$D_m \approx \frac{1}{|k\beta|_p} \quad (10)$$

If the degree of feedback is small, then it is necessary to consider the change in the phase angle of the loop transfer coefficient with frequency. Within the limits of the

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horizontal part of the amplitude-frequency characteristics
of the loop this angle changes according to the law:

$$\varphi = -2(1 - a) \arcsin \frac{f_i}{f_0}$$

where f_i is the frequency under consideration, f_0 is
the cut-off frequency.

Also, after determination of $|1 - k\beta|$, we obtain:

$$D_m = \frac{1}{\left\{1 + |k\beta|_p^2 + 2|k\beta|_p \cos[2(1 - a) \arcsin mx]\right\}^{1/2}} \quad (11)$$

where $x = f/f_0$ and f is the modulation frequency for
which the distortions are determined.

b) The examined frequency harmonic mf is greater than f_0 .

Then:

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$$|k\beta| = \frac{|k\beta|_p}{\left[\frac{mf}{f_0} + \sqrt{\left(\frac{mf}{f_0}\right)^2 - 1} \right]^{2(1-a)}}, \quad \arg(\bar{k}\bar{\beta}) = -180^\circ(1-a)$$

and:

$$D_m = \frac{1}{\left\{ 1 + \left(\frac{|k\beta|_p}{z_m} \right)^2 + 2 \frac{|k\beta|_p}{z_m} \cos[180^\circ(1-a)] \right\}^{1/2}} \quad (12)$$

where:

$$z_m = \left[mx + \sqrt{(mx)^2 - 1} \right]^{2(1-a)} \quad \text{and} \quad x = f/f_0.$$

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From Eq.(12), it is seen that values $D_m > 1$ are possible,
i.e. feedback can produce an increase in the harmonics instead
of compensating them.

Maximum D_m will be obtained at a modulation frequency
determined by:

$$z_{m \max} = \frac{|k\beta|_p}{-\cos[180^\circ(1-a)]} \quad (13)$$

when:

$$D_{m \max} = \frac{1}{\sin[180^\circ(1-a)]} \quad (14)$$

If the phase stability margin is taken $a = 1/6$ ($\psi = 30^\circ$)
then, from Eqs.(13) and (14), we find:

$$D_{m \max} = 2, \quad z_{m \max} = \frac{2}{\sqrt{3}}|k\beta|_p \quad \text{and} \quad (mx)_{\max} = \frac{z_{m \max}^{3/5} + z_{m \max}^{-3/5}}{2}.$$

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With a smaller stability margin, increase of non-linear distortions will be more significant.

Turning to Figure 3, where the curve of the step cutoff $|k\beta|$ is shown as a function of z , $|k\beta| = |k\beta|_p / z$, it is

easy to believe that the point $z_{m \max}$ is actually situated

in the limits of the falling part of the dislocation characteristic, if the phase stability margin is taken as $a = 1/6$ and the amplitude stability margin $b \geq 1.2$ db

$$(|k\beta|_{z_{an}} \leq \sqrt{3} / 2).$$

Thus, change of the loop transfer coefficient after frequency f_0 in accordance with the curves of an ideal

dislocation leads to increase of harmonics of the modulation frequency, falling in the region of frequencies close to $z_{m \max}$. If these harmonics comprise a significant part of

the distortions in the apparatus without feedback, then connection of feedback will lead to an increase of non-linear

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distortions.

In figure 4 are produced Curves $D_m = f(mx)$, calculated by Eqs.(11) and (12) with $a = 1/6$ and two values of feedback $|k\beta|_p = 20$ db and 26 db. From the figure, it is seen that, in the first case, only those harmonics which fall in the region of frequencies $mx < 1.61$ are compensated and, in the second case, this region is extended to $mx < 2.30$. The necessary value of the margin can be found from Eq.(12) by giving a value to D_m at the frequency $f_{p \max}$. So, if it is required that at frequency $f_{p \max}$ the feedback neither increases nor compensates the distortions, i.e. $(D_m)_{f=f_{p \max}} = 1$ then with $a = 1/6$, we obtain:

$$\frac{f_a}{f_{p \max}} = \frac{2m}{\left(\frac{|k\beta|_p}{\sqrt{3}}\right)^{3/5} + \left(\frac{|k\beta|_p}{\sqrt{3}}\right)^{-3/5}} \quad (15)$$

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Assuming that $(D_m)_{f=f_{p \max}} = 0.5$, i.e. demanding that at the highest modulation frequency the feedback reduces the harmonic, producing the distortions, twofold then:

$$\frac{f_o}{f_{p \max}} = \frac{2m}{\left(\frac{2|k\beta|_p}{\sqrt{3} + \sqrt{15}} \right)^{3/5} + \left(\frac{2|k\beta|_p}{\sqrt{3} + \sqrt{15}} \right)^{-3/5}} \quad (16) .$$

Results of calculations by Formulae (15) and (16) for the two values of m and $|k\beta|_p$ are given in the table. The relationships produced and the data of the table allow the frequency band margin necessary to ensure effective action of feedback at all frequencies to be found approximately.

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Compensation of Non-linear Distortions by Envelope Feedback in
Radio-transmitting Equipment

There are 4 figures, 1 table and 6 Soviet references.

SUBMITTED: June 8, 1957

Card 17/17 1. Radio transmitters--Distortion 2. Feedback amplifiers--
Applications 3. Mathematics--Applications

KANTOR, L.; KHATSKELEVICH, V.; SHUR, L.

Letters to the editors. *Elektrosviaz'* 12 no.12:74-75 D '58.
(MIRA 11:12)
(Radio--Transmitters and transmission)

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S/111/60/000/006/002/002
B019/B058

6.4500

AUTHORS: Khatskelevich, V. A., Docent, Candidate of Technical
Sciences, Yakovlev, L. N., Engineer

TITLE: An Instrument for Measuring the Input Resistance of
Broadcasting Antennas for Long and Medium Waves

PERIODICAL: Vestnik svyazi, 1960, No. 6, pp. 12 - 14

TEXT: An instrument is described here with which the reactive and active component of the internal resistance of an antenna-feeder device in the range of from 10 to 100 ohms may be determined. The wave range is between 200 and 2,000 m. It operates by the resonance method and consists of a generator, a power amplifier, a measuring circuit and 2 indicators. The block diagram is shown in Fig. 1, the detailed diagram in Fig. 2. The weak generator operates with an inductive feedback, the power amplifier is a cathode follower and the measuring circuit is connected with the power amplifier by a high-frequency transformer. The parasitic capacitances are the main cause of errors of measurement and their reduction through constructional measures is discussed. The measuring

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An Instrument for Measuring the Input
Resistance of Broadcasting Antennas for Long
and Medium Waves

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circuit is provided with a resistance box and the authors discuss the construction in detail. The capacitance box is also described in detail. The voltage at the primary coil of the transformer and the tuning are measured by the 2 indicators. The rectifier circuit (Fig. 4) is discussed next, the measuring process is described finally, and some practical advice is given. A checkup in a laboratory produced satisfactory results. There are 5 figures. ✓

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KHATSKELEVICH, Viktor Abramovich; FOMICHEV, I.N., otv. red.; LIBERZON,
L.G., red.; ROMANOVA, S.F., tekhn. red.

[Calculation of the performance of new generator triodes] Ras-
chet rezhimov novykh generatornykh triodov. Moskva, Gos. izd-
vo lit-ry po voprosam sviazi i radio, 1961. 48 p.
(MIRA 15:2)

(Oscillators, Electron-tube)
(Triodes)

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A055/A127

9.2510 (1003, 1020, 1067)

AUTHORS: Khatskelevich, V. A., Benben, G. V.

TITLE: Increasing the power amplification factor of the transmitter stages

PERIODICAL: Elektrosvyaz', no. 12, 1961, 62 - 64

TEXT: The number of h-f stages of a transmitter can be reduced by increasing as far as possible the power amplification factor of the last stages. For long and medium waves, using the common-cathode arrangement, it is still recommended to choose the power amplification factor K_p of a triode amplifier stage about equal to 10, i.e.:

$$K_p = \frac{P_{\text{ampl}}}{P_{\text{exc}}} \approx 10, \quad (1)$$

P_{ampl} being the oscillating power of the amplifier, and P_{exc} the power of its exciter. In the case of multigrid amplifier tubes, $K_p \approx 15 + 20$ etc. However, the "concealed power" in the tubes is such that it is sometimes possible to increase considerably the amplification factor and to bring it to 100, and even more instead of 10. Particularly important, from this point of view, is the calculation of the amplifier grid-circuit, especially in the case of new tubes. For this

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calculation, the authors refer to the method of V. A. Khatskevich [Ref. 3: "Elektricheskiy raschet rezhimov novykh generatornykh triodov" ("Electric calculation of the operating conditions of new oscillator tubes"), Radiotekhnika, 1959, no. 3]. This method, developed for new triodes, can also be applied to other tubes, and particularly to tubes of older types; it is sufficient to change the empiric correction coefficients and to state:

$$k_{0g} \approx 0.35 \div 0.55, \quad k_{1g} \approx 0.4 \div 0.6. \quad (3)$$

The greatest effect, as regards the increase of K_p , can be obtained with tubes having a small grid current, for instance the older types "Г-433" ("G-433") and also some of the more recent types, such as "ГY-4A" (GU-4A), "ГY-89A" (GU-89A) etc. The experimental check of the possibility of obtaining high values of K_p was therefore carried out with such tubes. A medium-wave 7-stage AM-transmitter with grid-bias-modulation in the stage preceding the penultimate one was used in the tests (the three last stages were push-pull stages). The last stage (amplifier of modulated oscillations) contained 6 "G-433" tubes giving an oscillating power $P_{\sim T} \approx 100$ kw in the telephone point, and a power $P_{\sim \max} = 4P_{\sim T} \approx 400$ kw in the peak point (at $m = 1$). The penultimate stage contained two 20 kw-"Г-431" (G-431) tubes,

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and the grid-bias modulation stage two 3 kw-"PK-3000" (OK-3000) tubes. The tubes of the last and penultimate stages satisfied, according to their rated characteristics, the condition $K_p \approx 10$. Calculation showed however the existence of a very great "power reserve" in these stages. A new penultimate stage was therefore designed, using four 750 watt-"6Y-80" (6U-80) tubes (operating in push-pull also). Even at a screen-grid voltage $E_{g2} \approx 500$ v (instead of the rated 600 v), this new penultimate stage permitted easily the former operation of the last stage. The power of the penultimate stage in the "telephone point" being $P_T \approx 600$ watts, the power amplification factor of the last stage was

$$K_p = \frac{P_{T \text{ last st.}}}{P_{T \text{ penult. st.}}} \approx \frac{100 \cdot 10^3}{600} \approx 170 \quad (!!)$$

There are 3 figures and 3 Soviet-bloc references. The following names of Soviet-bloc authors or scientists are mentioned in the article: A. M. Pisarevskiy, I. E. Sirekin and E. I. Belen'kiy.

SUBMITTED: March 1, 1961

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KHATSKELEVICH, Viktor Abramovich; PISAREVSKIY, A.M., red.; ZHITNIKOVA,
O.S., tekhn. red.

[Calculation of the operation of a plate modulated oscillator
using new types of electron tubes] Raschet rezhimov generatora
pri anodnoi moduliatsii na novykh lampakh. Moskva, Gosenergo-
izdat, 1962. 109 p. (MIRA 16:3)
(Oscillators, Electron-tube)

1984-1985

Radio tekhnika i elektronika

Svetokalevich, V. A.; Vorob'ye, V. I.

On an experimental vhf transmitter

Radio tekhnika i elektronika, No. 1, 1984, pp. 1-4

English translation: 1984, 1985

The article describes the construction and operation of a VHF transmitter. The transmitter is based on a vacuum tube and is designed for operation in the VHF range. The authors describe the circuitry, components, and the results of the experimental work. The transmitter is capable of operating at various frequencies and has a high power output. The authors also discuss the advantages and disadvantages of the transmitter and provide a detailed description of its construction and operation.

KHATSKEVICH, K.M.; KASHTELIAN, S.F.

Role of the cytogram of wounds exudate in wound sepsis. Medych.
zhur. 17:317-322 '47. (MIRA 11:1)

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